

Lecture 8: Linear Errors & Corrections

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“.. it turns out that in the presence of nonlinear perturbations only rational frequencies $Q = p/q$ with $q = 2$ or 3 , or sometimes 4 , lead to instability. Therefore, it is possible to design machines with stable orbits by ensuring that the tunes avoid these values.”

E. Courant, “Accelerators, Colliders, and Snakes”.

A) TUNE PLANE (INTRO.)

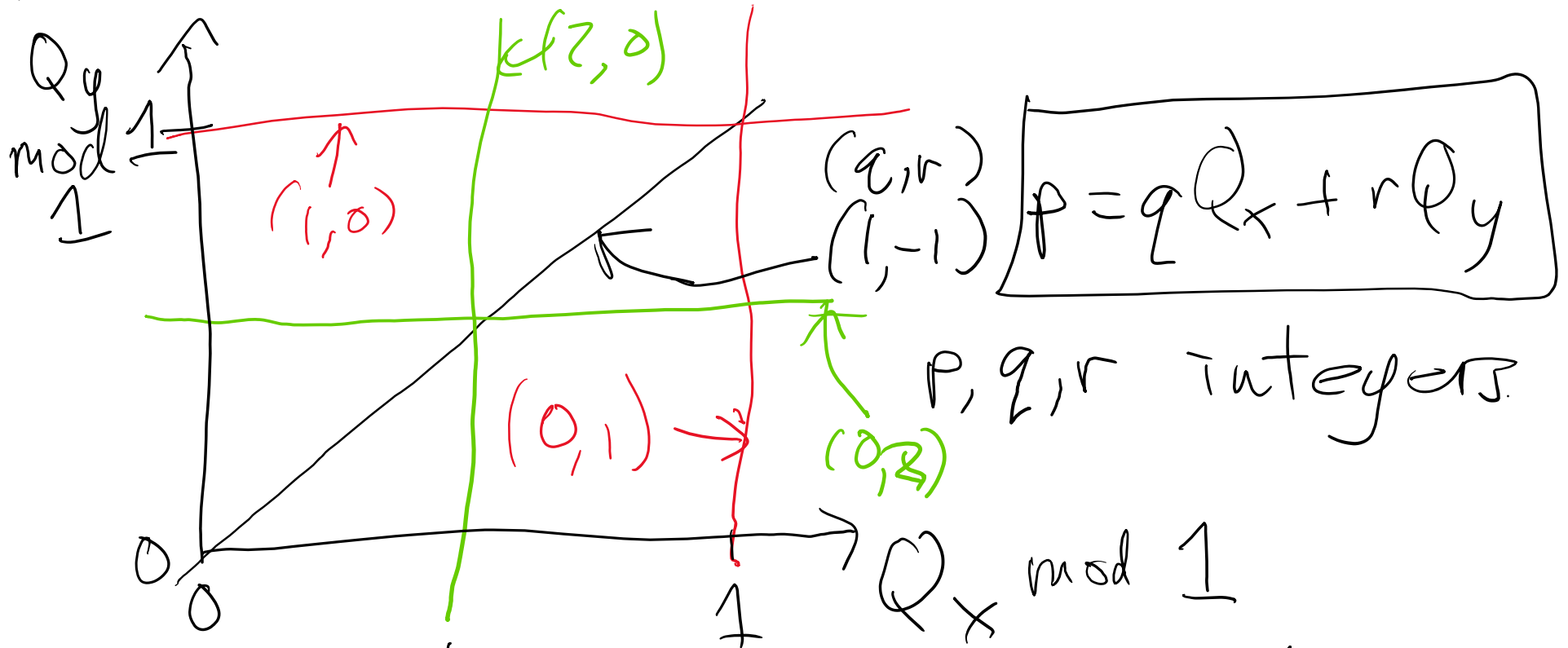
B) TRAJECTORY & CLOSED ORBIT

C) H-V COUPLING

D) QUAD STRENGTH ERRORS

HIDDEN AGENDA = INTRO TO RESONANCES

A) TUNE PLANE INTRO.



- p can be very large... but often just the integer parts of $Q_x + Q_y$

B) TRAJECTORY & CLOSED
ORBIT

Take a multipole magnet

$$B_y + iB_x = C_n (x + iy)^n$$

C_0 : dipole

C_1 : quad

C_2 : sext

DISPLACE $x \rightarrow x + \Delta x, y \rightarrow y + \Delta y$

$$B_y + iB_x = C_n \left[(x + iy)^n - n(x + iy)^{n-1} (\Delta x + i\Delta y) + \dots \right]$$

QUADRUPOLE

FEED DOWN

E.G. $f = 10 \text{ m}, \Delta x = 1 \text{ mm}$

$$\Delta x' = \frac{x}{f} + \frac{\Delta x}{f}$$

$$\Rightarrow \Delta x'/f = 100 \text{ } \mu\text{rad}$$

CONSTANT

TERM :

DIPOLE !!

DIPOLE ROLL (Displacements do nothing)

E.G. A dipole of θ angle is rolled about the longitudinal axis by α

$$\Delta y' = \alpha \theta \quad [\text{CONSTANT}]$$

E.G. $\theta = 40 \text{ } \mu\text{rad}$, $\alpha = 1 \text{ } \mu\text{rad}$

$$\Rightarrow \Delta y' = 40 \text{ } \mu\text{rad}$$

So: a single misaligned magnet (dipole or quadrupole) generates angle kicks $\sim 100 \text{ } \mu\text{rad}$, $\pm 1 \text{ eV}$

Q1: How bad is this?

Q2: How to correct it?

Q3: Free wave or closed orbit (with PBC)?

FREE WAVE In a transfer line or linac

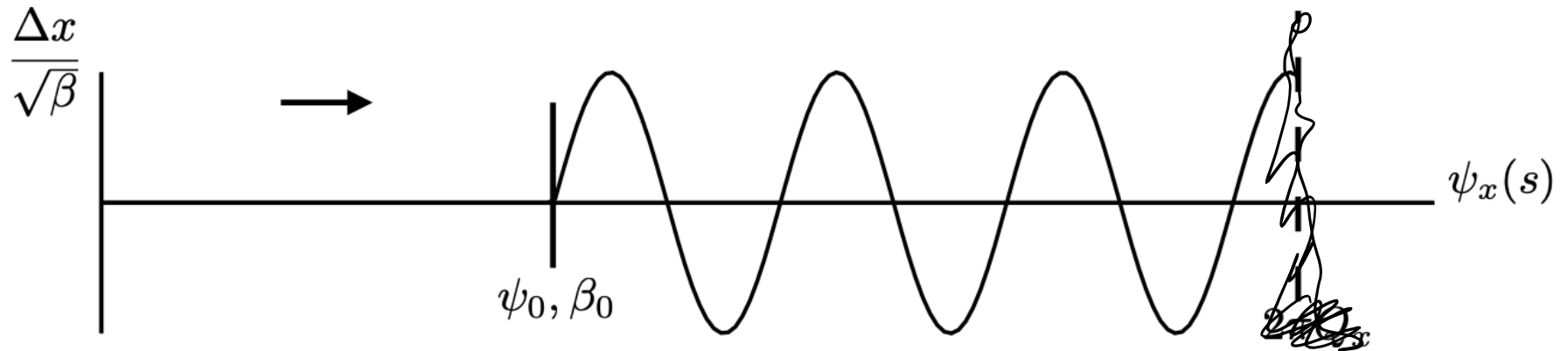
$$\frac{x}{\sqrt{\beta}} = \Delta x' \sqrt{\beta_0} \cdot \sin(\psi(s) - \psi_0) \quad s > s_0$$

EG, $\Delta x' = 10^{-4}$ radians, $\beta = 50$ m (large..?)

$$\langle x^2 \rangle^{1/2} \approx 5 \text{ mm}$$

Can't take many such (uncorrected) errors
before beam hits beam pipe !!

8.1 Downstream free wave response to an angular kick error.



Q: What happens in a storage ring with PBC?

CLOSED ORBIT ERRORS

$$\begin{pmatrix} x \\ x' \end{pmatrix}_{co} = M \begin{pmatrix} x \\ x' \end{pmatrix}_0 + \begin{pmatrix} 0 \\ \Delta x' \end{pmatrix}$$

$$\text{so } \begin{pmatrix} X \\ X' \end{pmatrix}_{CO} = (I - M)^{-1} \begin{pmatrix} 0 \\ \Delta X' \end{pmatrix}$$

I = Identity 2×2

WATCH OUT if $\det(I - M) \rightarrow 0$!!

$$(I - M)^{-1} = \frac{1}{2(1 - C)} \begin{pmatrix} 1 - C & \beta S \\ -\frac{S}{\beta} & 1 - C \end{pmatrix}$$

$$C = \cos(2\pi Q_x)$$

$$S = \sin(2\pi Q_x)$$

watch out for
 $C = 1 = Q_x = 0, 1, 2, \dots$

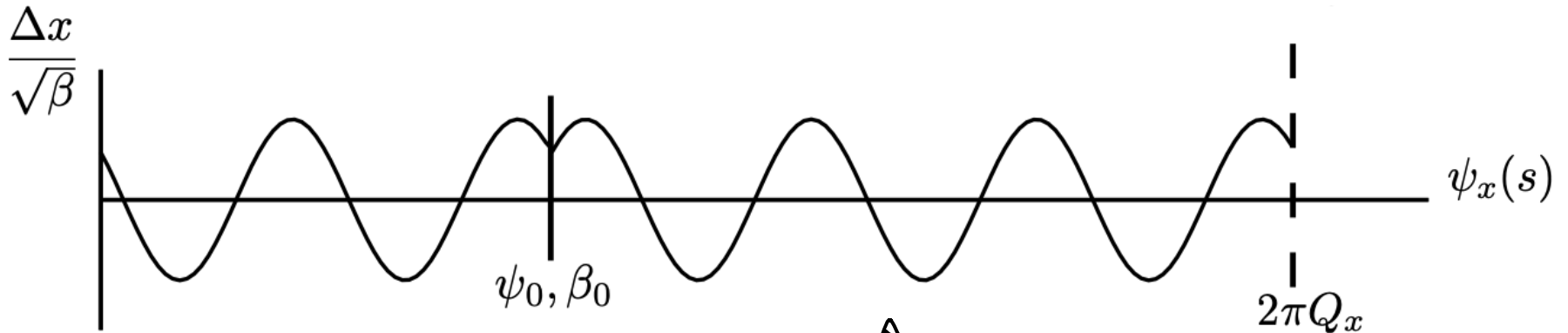
AT KICK LOCATION

$$\begin{pmatrix} x \\ x' \end{pmatrix}_{CO} = \frac{\Delta x'}{2\sin(\pi Q_x)} \begin{pmatrix} \beta_0 \cos(\pi Q_x) \\ \sin(\pi Q_x) - \alpha_0 \cos(\pi Q_x) \end{pmatrix}$$

for any α_0

resonance denominator

8.2 Closed orbit wave response to an angular kick.



At ANY location

$$\frac{x_{co}}{\sqrt{\beta}} = \frac{\Delta x' \sqrt{\beta_0}}{2 \sin(\pi Q_x)} \cdot \cos(|\psi - \psi_0| - \pi Q_x)$$

Shows that $\sqrt{\beta}$ or $\sqrt{\beta_0}$ is a "sensitivity" measure
 TUNES WITH $\mu \approx Q_x$ are dangerous
RESONANCE EXAMPLE 1 $(q, r) = (1, 0)$
 $(0, 1)$ 12

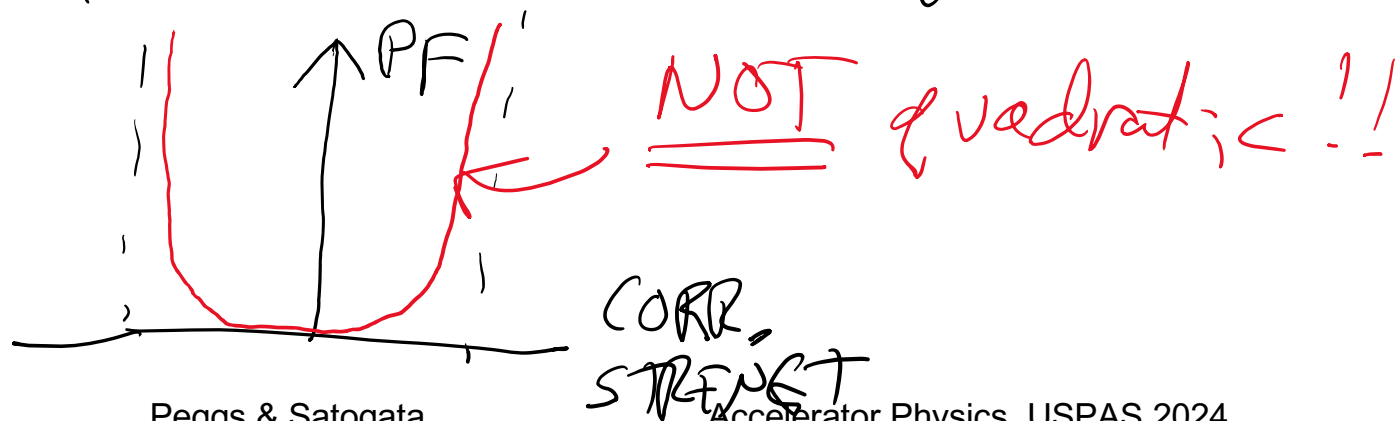
CLOSED ORBIT CORRECTION

- 1) Measure C.O. location at many BPMs
- 2) Correct by powering many weak dipole correctors

THERE ARE MANY ALGORITHMS

to solve this linear problem.

- Q1: What is the penalty function? PF
- Q2: What about dipole corrector limits?
- Q3: Must we use 19th century tools?



ONE OF MANY ALGORITHMS is the
"SLIDING 3-BUMP" which allows any PF

Downstream of 3 dipole correctors 1, 2, 3

$$\frac{x(\psi)}{\sqrt{\beta}} = \sum_{i=1}^3 x_i' \sqrt{\beta_i} \cdot \sin(\psi - \psi_i)$$

IF this sum is zero, no need to apply PBC!

\Rightarrow displacements are localised to
 $\psi_1 < \psi < \psi_3$

3-BUMP localization is guaranteed if

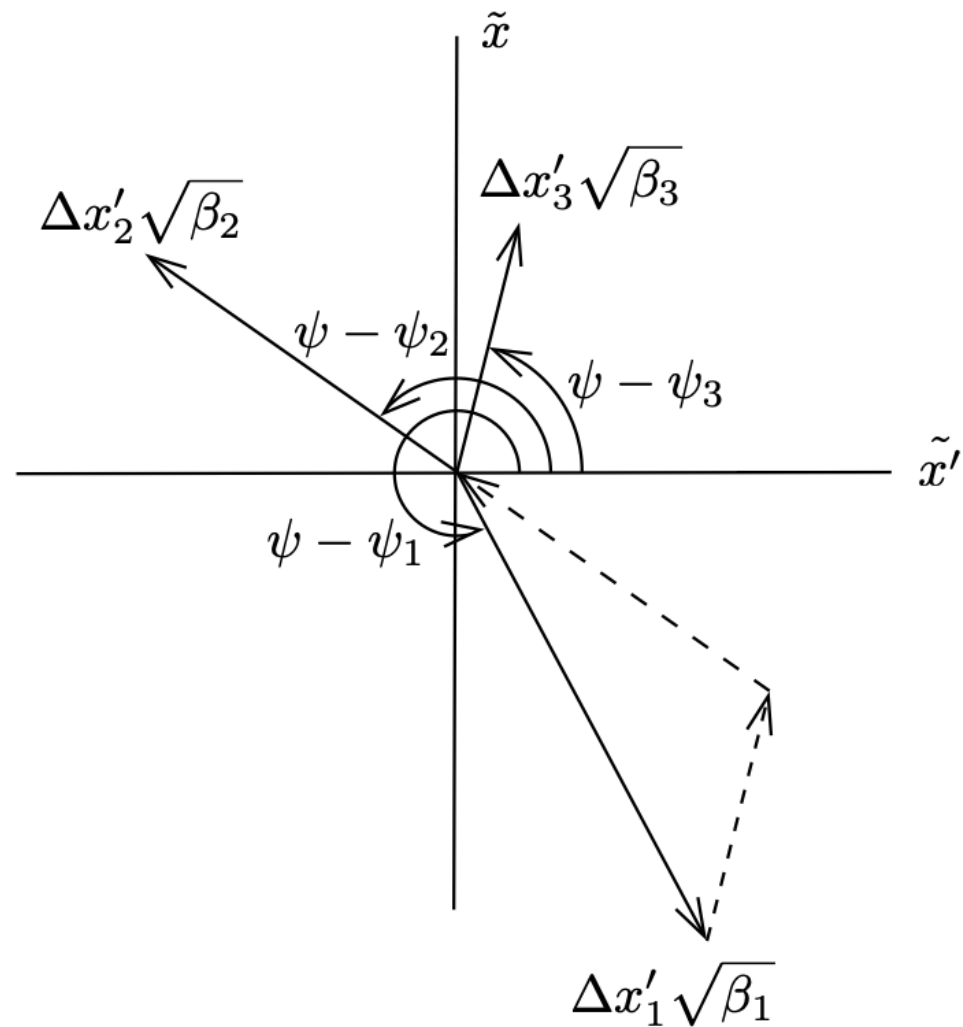
$$\frac{\Delta x_i \sqrt{\beta_i}}{\sin(\psi_j - \psi_k)} = \kappa$$

for (i, j, k) cyclic combination of $(1, 2, 3)$

Adjust bump strength κ for $(1, 2, 3)$ to minimize local PF, then $(2, 3, 4)$, then $(3, 4, 5)$ et cetera.

REPEAT until global PF is minimized
- Correction repetition is often necessary in the control room, as well as in calculation.

8.4 Three-bump vectors rotating in normalized phase space, always adding to zero.



C) H-V COUPLING

ROLLED QUADS

LINEAR COUPLING - ROLLED QUADS

Roll ANY magnet with 4×4 matrix M
by angle α

$$M_{\text{ROLLED}} = R(-\alpha) M R(\alpha)$$

where $R = \begin{pmatrix} c & 0 & s & 0 \\ 0 & c & 0 & s \\ -s & 0 & c & 0 \\ 0 & -s & 0 & c \end{pmatrix}$

$$c = \cos(\alpha) \approx 1$$

$$s = \sin(\alpha) \approx \alpha$$

so a Rolled Thin Quad becomes

$$M_{\text{RTQ}} \approx M_{\text{TQ}} + \alpha \begin{pmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & -2g & 0 \\ \hline 0 & 0 & 0 & 0 \\ -2g & 0 & 0 & 0 \end{pmatrix}$$

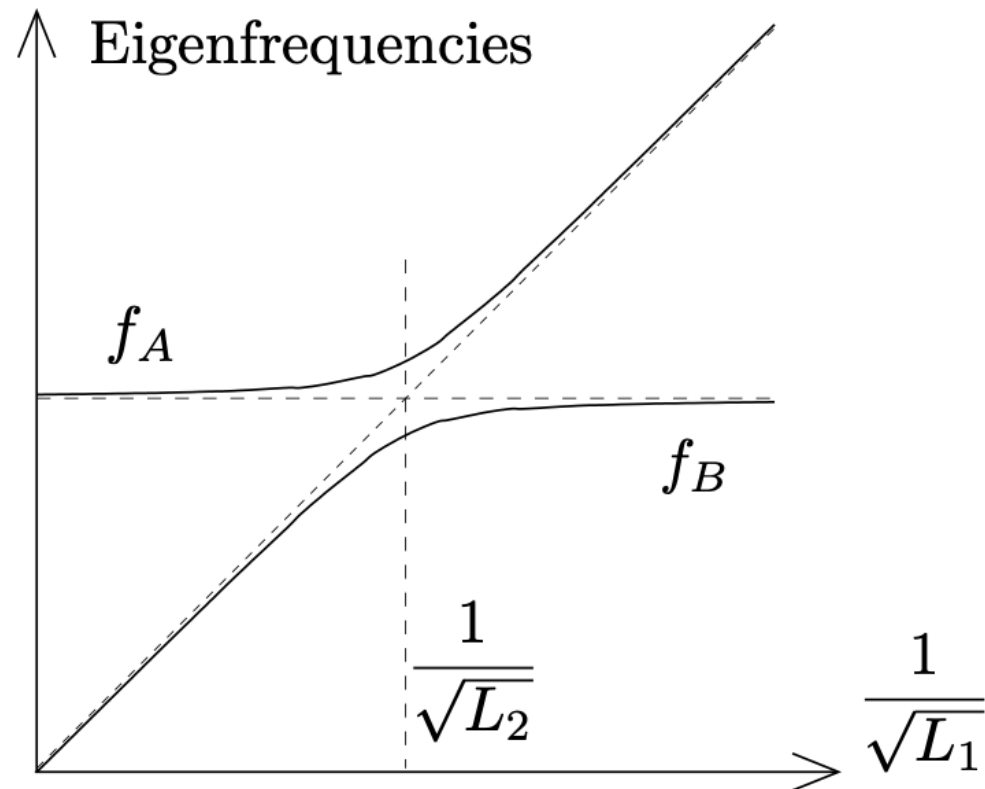
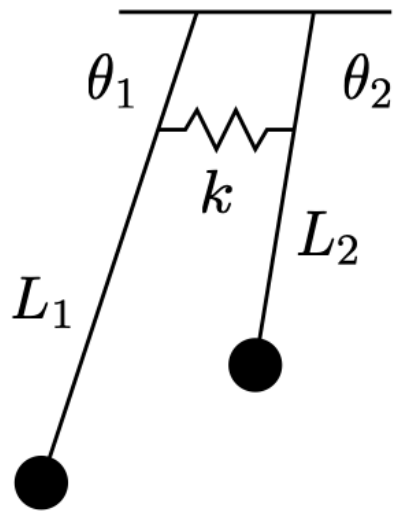
COUPLING
H & V
motion !!

ANALOGY: 2 weakly coupled pendula

No coupling: $f_1 \sim 1/\sqrt{L_1}$, $f_2 \sim 1/\sqrt{L_2}$

WITH COUPLING ... vary L_1 across values of L_2

8.5 The eigenfrequencies of two weakly coupled pendula as the length L_1 is varied.



WITH coupling, still have 2 eigenfrequencies $f_A + f_B$

$$\theta_1 = a_{1A} \cos(f_A t + \phi_{1A}) + a_{1B} \cos(f_B t + \phi_{1B})$$

$$\theta_2 = a_{2A} \cos(f_A t + \phi_{2A}) + a_{2B} \cos(f_B t + \phi_{2B})$$

- f_A is always $> f_B$
- There is a ~~close~~ approach of $|f_A - f_B|$, depending on spring constant k

Similarly, H eV accelerator motion is coupled & confused if

$$|\rho + Q_x - Q_y| \lesssim Q_{\min}$$

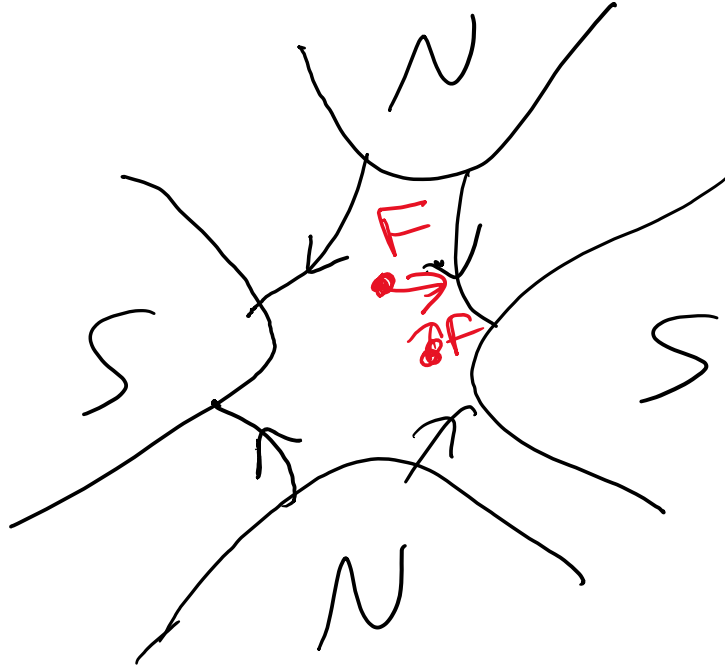
design tunes

$Q_{\min} \approx 0.001$
well tuned

or
badly tuned

RESONANCE EXAMPLE 2 : $(l, r) = (1, -1)$

CORRECT COUPLING WITH SKEW QUADS



IN CONTROL ROOM:

→ {
measure Q_{min}
tweak skew quad 1, 2
}

eg
CESR
SPS

D) QUAD STRENGTH ERRORS

TUNE SHIFTS & β -WAVES

Suppose a quad at s_0 has a strength error

$$\Delta q = \Delta \left(\frac{1}{f} \right)$$

- Q1) Is the motion still stable? If yes...
- Q2) How much do Q_x & Q_y change?
- Q3) What happens to β -functions everywhere?

One turn matrix becomes

$$\tilde{M} = M \begin{pmatrix} 1 & 0 \\ -\Delta q & 1 \end{pmatrix}$$

and perturbed tune is found by solving

$$\text{Tr}(\hat{M}) = 2\cos(2\pi\hat{Q})$$

or

$$\cos(2\pi\hat{Q}) = \cos(2\pi Q) - \frac{\beta_0 \Delta q}{2} \sin(2\pi Q)$$

- Exact!

- β_0 is a sensitivity factor

A1: Motion is still stable if $|\text{Tr}(\hat{M})| \leq 2$

- If Δq is small, then

$$\Delta Q = \hat{Q} - Q = \frac{\beta_0 \Delta q}{4\pi}$$

- Δq has different signs in H & V
 $\Rightarrow \Delta Q_x$ & ΔQ_y have different signs
- E.g. 1% error in $f=10$ m quad
 with $(\beta_x, \beta_y) = (50, 10)$ m
 gives $(\Delta Q_x, \Delta Q_y) = (0.0040, -0.0008)$
- Tune shifts are easily corrected by
 the families of main arc F & D
 quad repoles
- β -function errors are TRICKIER!!

β -WAVES = FREE

JUST DOWNSTREAM of error quad

$$\begin{pmatrix} \Delta\beta \\ \Delta\alpha \\ \Delta\gamma \end{pmatrix} = \begin{pmatrix} 1 & 0 & 0 \\ \Delta q & 1 & 0 \\ (\Delta q)^2 & 2\Delta q & 1 \end{pmatrix} \begin{pmatrix} \beta \\ \alpha \\ \gamma \end{pmatrix}$$

launching a FREE WAVE

$$\frac{\Delta\beta}{\beta} = -\Delta q \cdot \beta_0 \sin(2(\psi - \psi_0))$$

TWICE the
peak of
phase
advance

E.G., $\Delta q = 10^{-2} \left(\frac{1}{10}\right)$, $\beta_0 = 50 \text{ m} \Rightarrow \approx 1\%$ error wave!

\Rightarrow Dangerous! Control at 10^{-4} level if possible.

β -WAVES; PBC

In a circular accelerator with PBC

$$\frac{\Delta\beta}{\beta} = \frac{-\Delta Q\beta_0}{2\sin(2\pi Q)} \cdot \cos(2|\psi - \psi_0| - 2\pi Q)$$

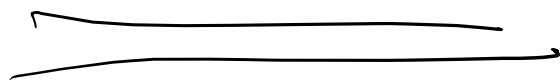
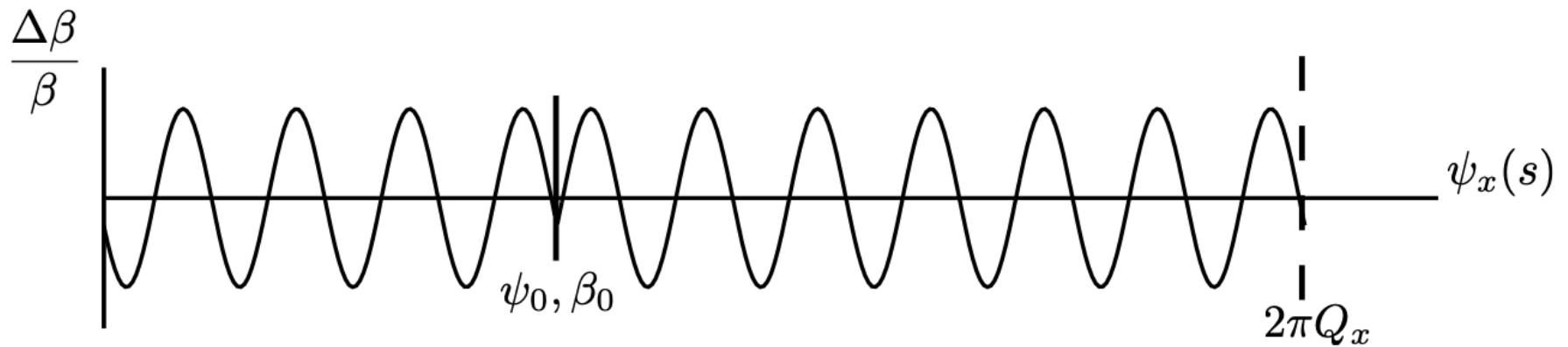
RESONANCE DENOMINATOR

RESONANCE EXAMPLES!

Optics are especially vulnerable to errors if $p \approx 2Q_x$, or $p \approx 2Q_y$

that is: $(\varrho, r) = (z, \theta)$ or (∂, \mathcal{R})

8.3 Closed beta wave response due to a quad strength error.



Q: Why also include NONLINEAR correctors??

Q: Where do higher order (nonlinear) resonances come from? . . .