

# USPAS Accelerator Physics 2024

## Hampton VA / Northern Illinois University

### Lattice Examples II

(or putting much of the week together)  
(or Even More Stupid Lattice Tricks)

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<http://www.toddsatogata.net/2024-USPAS>

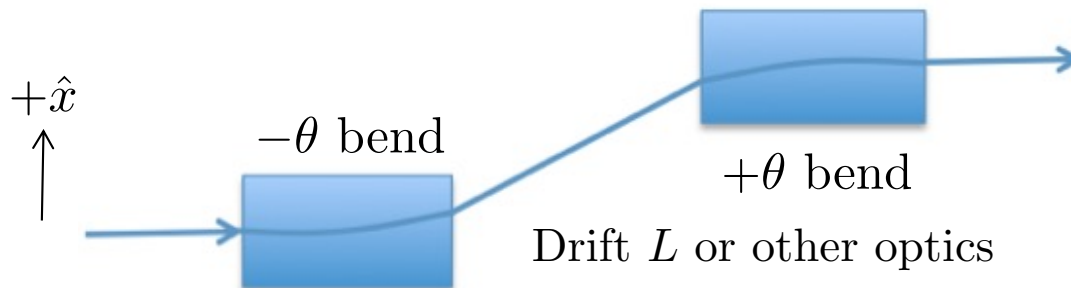
Happy Birthday to Polykarp Kusch (Nobel 1955; EDM), Paul Newman, and Wayne Gretzky!

Happy National Peanut Brittle Day, National Spouses Day, and Dental Drill Appreciation Day!

# Overview (Afternoon)

- Achromats
  - Doglegs and achromatic doglegs
  - Chicanes and bunch compressors
  - Double bend achromat
  - Triple bend achromat
  - (MAX-IV Multi-bend achromat; more Tuesday)
- 2D/3D manipulation:
  - Longitudinal/transverse emittance exchange

# Doglegs



- Displaces beam transversely without changing direction
- What is effect on 6D optics?

$$\mathbf{M}_{\text{dipole}}(\rho, \theta) = \begin{pmatrix} \cos \theta & \rho \sin \theta & 0 & 0 & 0 & \rho(1 - \cos \theta) \\ -\frac{1}{\rho} \sin \theta & \cos \theta & 0 & 0 & 0 & \sin \theta \\ 0 & 0 & 1 & \rho\theta & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ -\sin \theta & -\rho(1 - \cos \theta) & 0 & 0 & 1 & L/(\gamma^2 \beta^2) - \rho(\theta - \sin \theta) \\ 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix}$$

- Be careful about the coordinate system and signs!!
- If  $\rho, \theta > 0$ , positive displacement points **out** from dipole curvature
- Be careful about order of matrix multiplication!

# Reverse Bend Dipole Transport

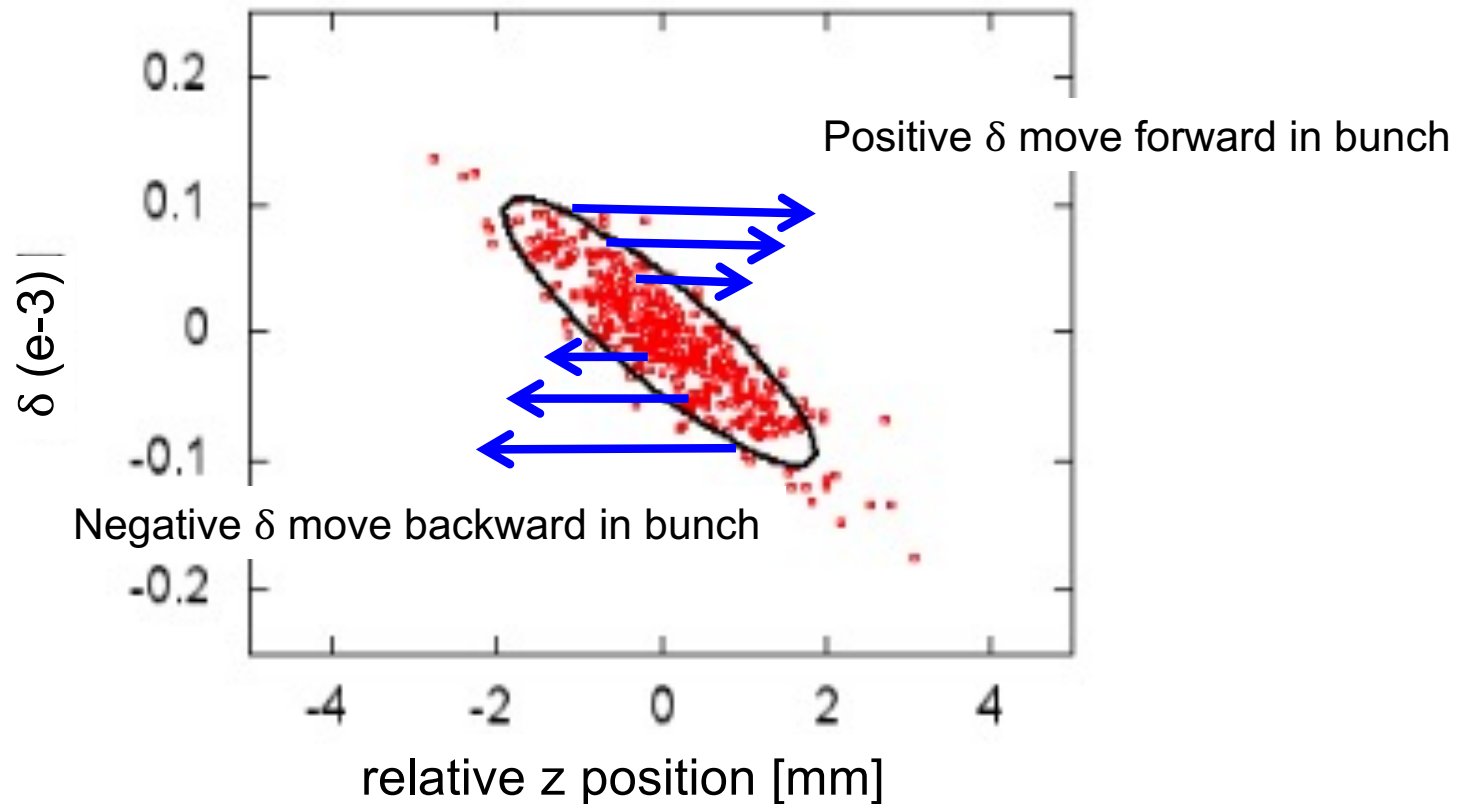
- What is the correct 6x6 transport matrix of a reverse bend dipole?
- It turns out to be achieved by reversing **both**  $\rho$  and  $\theta$ 
  - $\rho\theta=L$  (which stays positive) so both must change sign

$$\mathbf{M}_{\text{dipole}}(-\rho, -\theta) = \begin{pmatrix} \cos \theta & \rho \sin \theta & 0 & 0 & 0 & -\rho(1 - \cos \theta) \\ -\frac{1}{\rho} \sin \theta & \cos \theta & 0 & 0 & 0 & -\sin \theta \\ 0 & 0 & 1 & \rho\theta & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ \sin \theta & \rho(1 - \cos \theta) & 0 & 0 & 1 & L/(\gamma^2 \beta^2) - \rho(\theta - \sin \theta) \\ 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix}$$

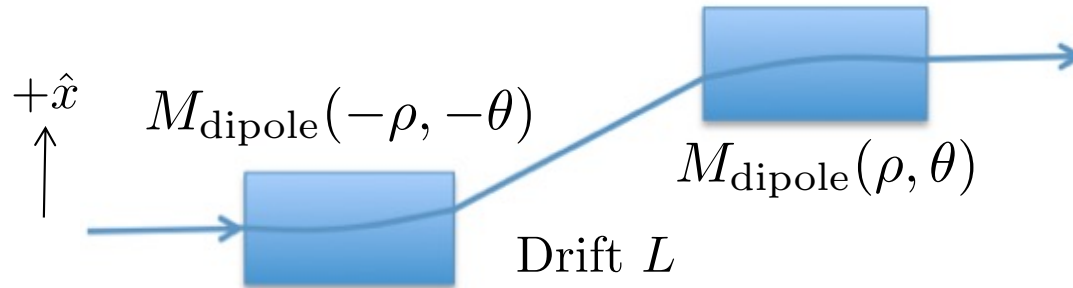
$$\mathbf{M}_{\text{drift}} = \begin{pmatrix} 1 & L & 0 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 & 0 & 0 \\ 0 & 0 & 1 & L & 0 & 0 \\ 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & L/(\gamma^2 \beta^2) \\ 0 & 0 & 0 & 0 & 0 & 1 \end{pmatrix}$$

# Aside: Longitudinal Phase Space Drift

- Wait, what was that  $M_{56}$  term with the relativistic effects?
  - Recall longitudinal coordinates are  $(z, \delta)$
  - This extra term is called “ballistic drift”: not in all codes!
    - Important at low to modest energies and for bunch compression
    - Relativistic terms enter converting momentum  $p$  to velocity  $v$



# Weak Dogleg



$$\mathbf{M}_{\text{dogleg}} = \mathbf{M}_{\text{dipole}}(\rho, \theta) \mathbf{M}_{\text{drift}} \mathbf{M}_{\text{dipole}}(-\rho, -\theta)$$

$$\mathbf{M}_{\text{weak dogleg}} = \begin{pmatrix} 1 & \rho\theta & \frac{\rho\theta^2}{2} \\ 0 & 1 & \theta \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & L & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & \rho\theta & \frac{\rho\theta^2}{2} \\ 0 & 1 & -\theta \\ 0 & 0 & 1 \end{pmatrix}$$

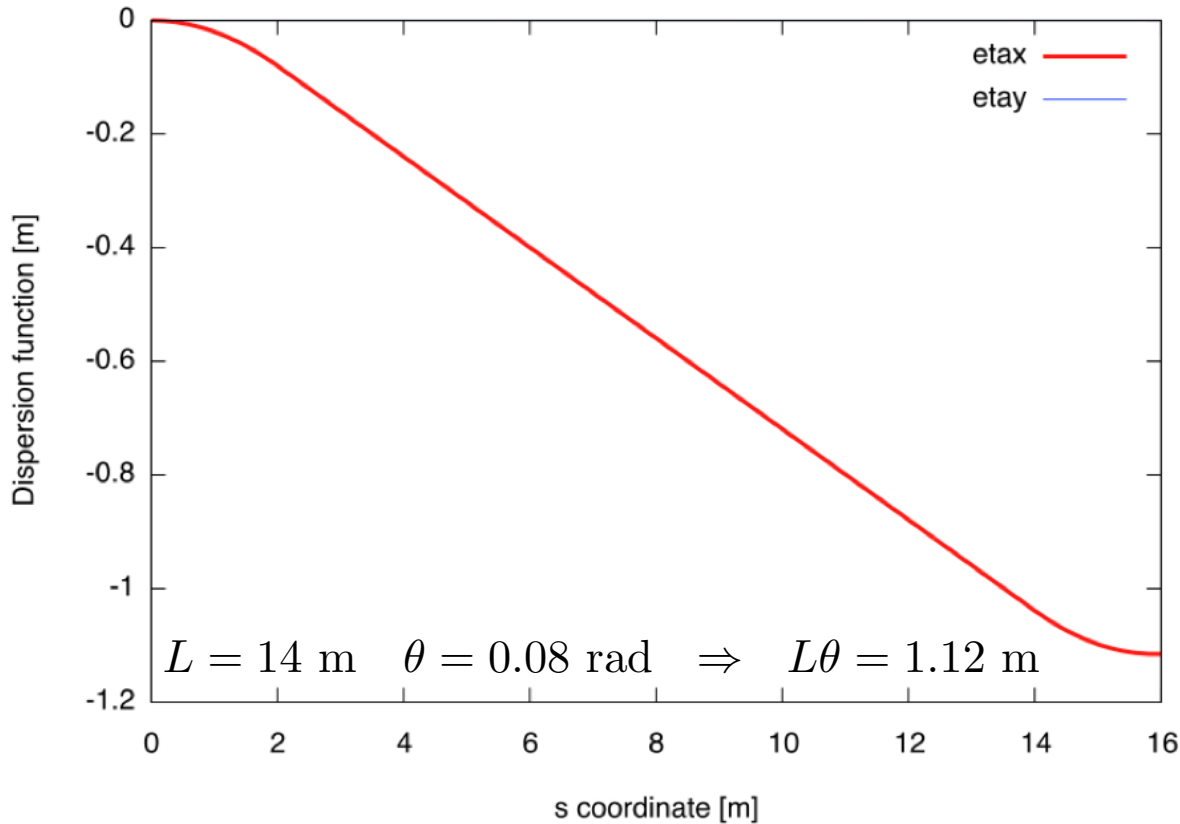
Check  
sign

$$= \begin{pmatrix} 1 & L + 2\rho\theta & -L\theta \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \Rightarrow (\eta, \eta')_{\text{in}} = 0 \\ \Rightarrow (\eta, \eta')_{\text{out}} = (-L\theta, 0)$$

Strong dogleg can also be derived:

$$D = -L \cos \theta \sin \theta \quad D' = \frac{L \sin^2 \theta}{\rho}$$

# Dogleg Dispersion



For weak dogleg

$$(\eta, \eta')_{\text{in}} = 0$$

$$\Rightarrow (\eta, \eta')_{\text{out}} = (-L\theta, 0)$$

Does this make sense?

$$\Delta x'(\delta) = \frac{BL}{(B\rho)} = \frac{q}{p(1+\delta)} [BL] \approx \frac{q}{p} [BL] (1-\delta) = (1-\delta) \Delta x'(\delta=0)$$

A small momentum offset of  $+\delta$  reduces the dipole kick by a factor of delta, and this is magnified to a transverse offset from design at the end of the dogleg by  $-\delta L\theta$ .

# Achromatic Dogleg

- How can we make an achromatic dogleg?

$$(\eta, \eta')_{\text{in}} = (0 \text{ m}, 0) \Rightarrow (\eta, \eta')_{\text{out}} = (0 \text{ m}, 0)$$

- Use an I insertion (e.g. four consecutive  $\pi/2$  insertions)

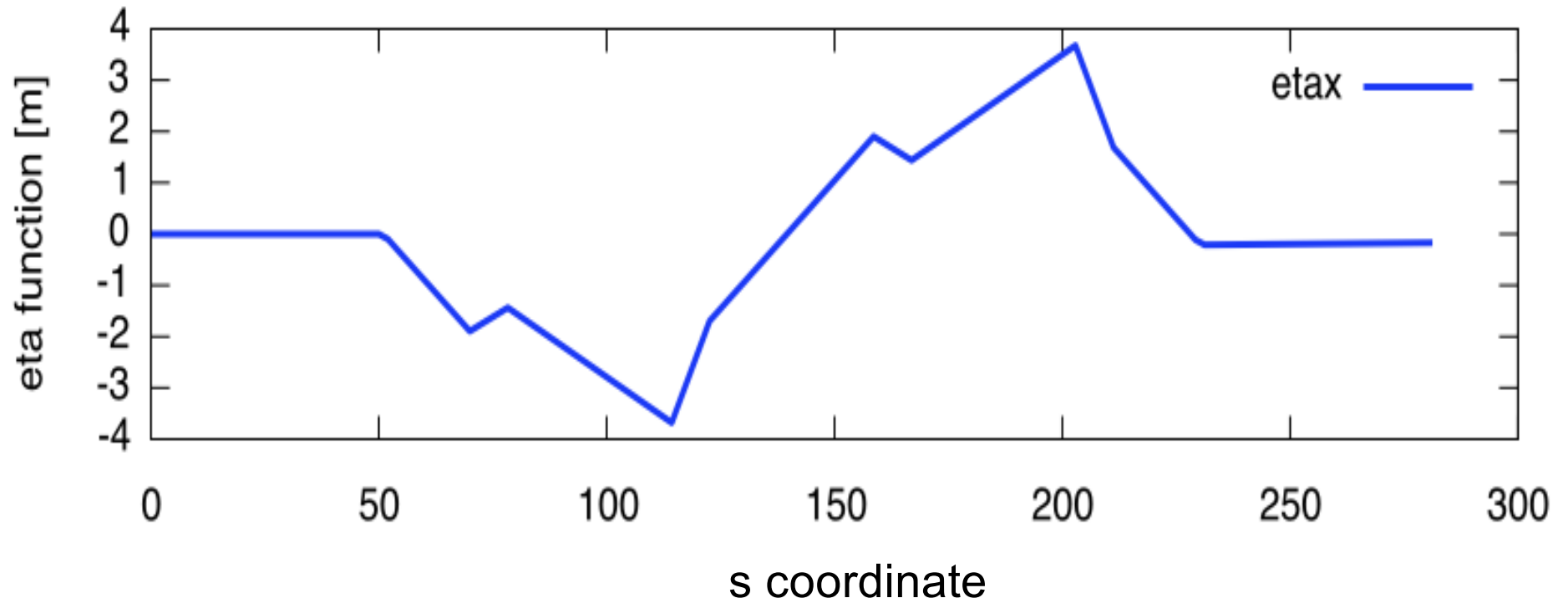
$$\mathbf{M}_{\pi/2} = \begin{pmatrix} \alpha & \beta \\ -\gamma & -\alpha \end{pmatrix} = \mathbf{J} \quad (\text{Recall } \mathbf{J}^4 = \mathbf{I})$$

$$\mathbf{M}_{\text{achromatic dogleg}} = \begin{pmatrix} \cos(2\theta) & \rho \sin(2\theta) & 0 \\ -\frac{\sin(2\theta)}{\rho} & \cos(2\theta) & 0 \\ 0 & 0 & 1 \end{pmatrix} \quad \text{achromatic!}$$

- Any** transport with net phase advance of  $2n\pi$  will be achromatic ( $n\pi$  if all dipoles bend in same direction)
  - common trick for matching dispersive bending arcs to non-dispersive straight sections.



# Achromatic Dogleg



# Achromatic Dogleg: Steffen CERN School Notes

## Example of nondispersive translating system

$\Phi$  = sector magnet bend. angle

$\varphi = \ell\sqrt{k}$  = quadrupole magnet phase angle

$d, \lambda$  = drift space lengths.

The system is nondispersive if the sinelike trajectory (with respect to the central symmetry point) goes through the mid-point of the bending magnets, i.e. if

$$\rho \tan \frac{\Phi}{2} + \lambda = \frac{1}{\sqrt{k}} \frac{d\sqrt{k} \cos \varphi + 2 \sin \varphi}{d\sqrt{k} \sin \varphi - 2 \cos \varphi}.$$

Focusing also in the other plane may be obtained by adding a third quadrupole of opposite polarity at the symmetry point.

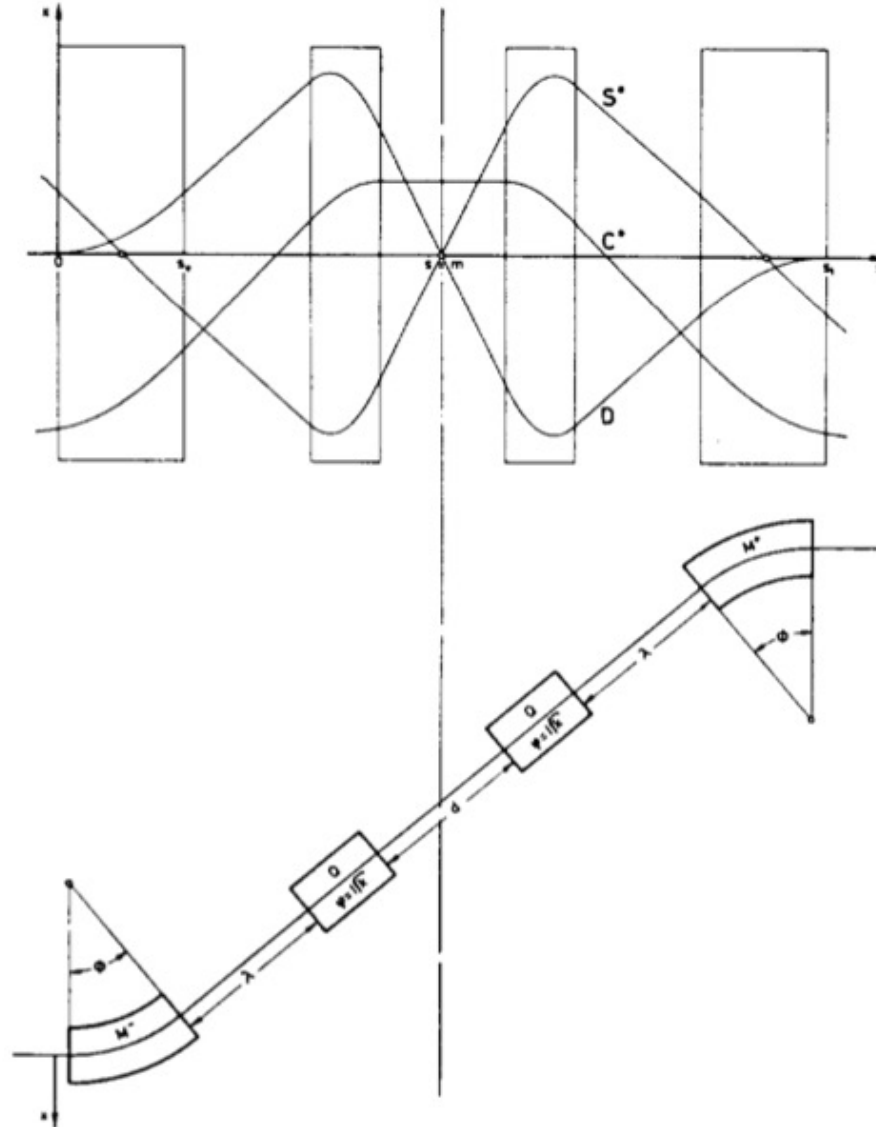


Fig. 15: Nondispersive translating system.

K. Steffen, CERN-85-19-V-1, 1985, p. 55

# First-Order Achromat Theorem

- A lattice of  $n$  repetitive cells is achromatic (to first order, or in the linear approximation) iff  $\mathbf{M}^n = \mathbf{I}$  or each cell is achromatic

- Proof:

Consider  $\mathbf{R} \equiv \begin{pmatrix} \mathbf{M} & \bar{d} \\ 0 & 1 \end{pmatrix}$  where  $\begin{pmatrix} x \\ x' \\ \delta \end{pmatrix}_2 = \mathbf{R} \begin{pmatrix} x \\ x' \\ \delta \end{pmatrix}_1$   $\bar{d} = \begin{pmatrix} M_{16} \\ M_{26} \end{pmatrix}$

For  $n$  cells :  $\mathbf{R}^n = \begin{pmatrix} \mathbf{M}^n & (\mathbf{M}^{n-1} + \mathbf{M}^{n-2} + \dots + \mathbf{I})\bar{d} \\ 0 & 1 \end{pmatrix}$

but  $(\mathbf{M}^{n-1} + \mathbf{M}^{n-2} + \dots + \mathbf{I}) = (\mathbf{M}^n - \mathbf{I})(\mathbf{M} - \mathbf{I})^{-1}$

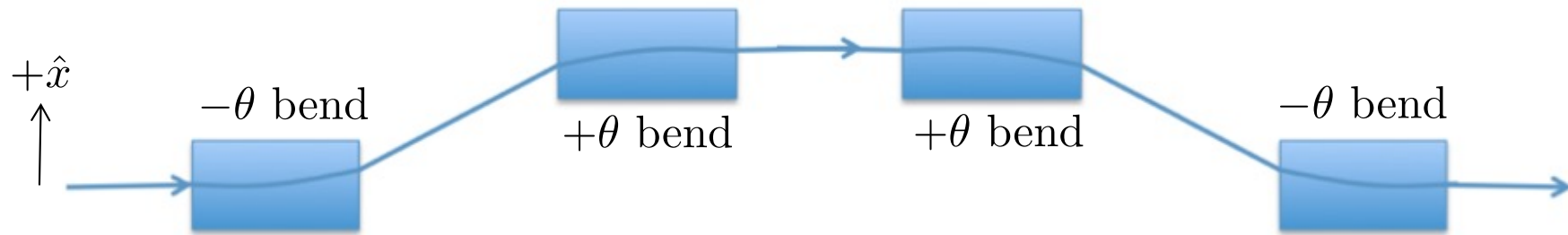
So for  $n$  cells :  $\mathbf{R}^n = \begin{pmatrix} \mathbf{M}^n & (\mathbf{M}^n - \mathbf{I})(\mathbf{M} - \mathbf{I})^{-1}\bar{d} \\ 0 & 1 \end{pmatrix}$

- So the lattice is achromatic only if  $\bar{d} = 0$  or  $\mathbf{M}^n = \mathbf{I}$

$$\mathbf{M}^n = \mathbf{I} \cos \mu_{\text{tot}} + \mathbf{J} \sin \mu_{\text{tot}} \Rightarrow \mu_{\text{tot}} = 2\pi k$$

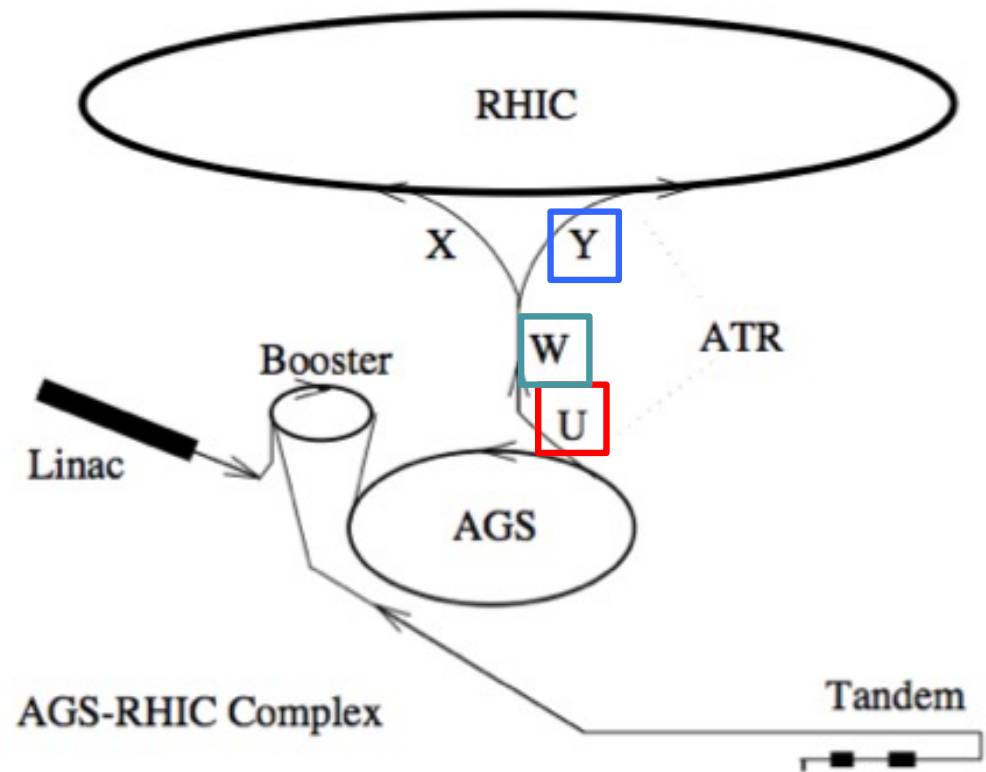
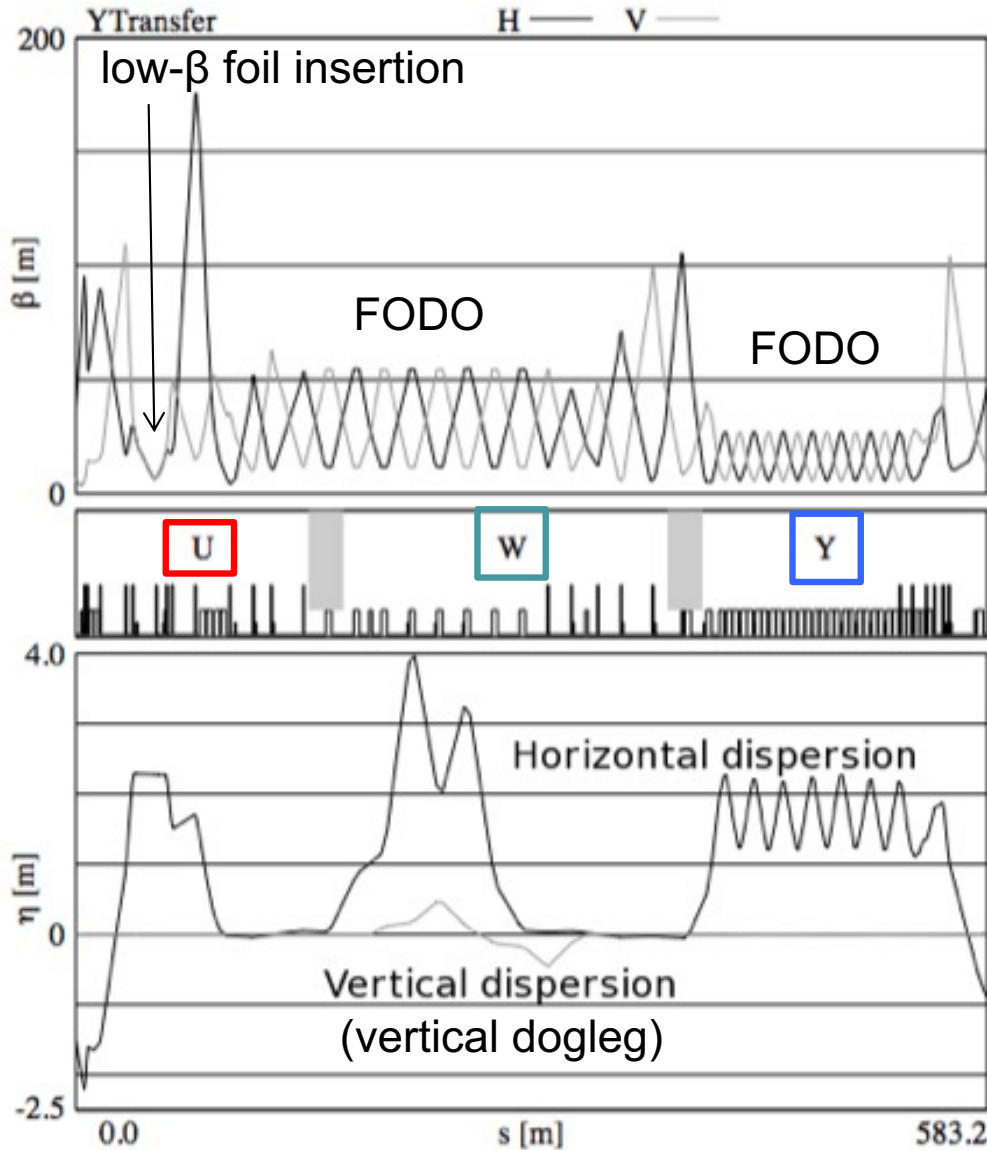
S.Y. Lee, "Accelerator Physics"

# Chicane



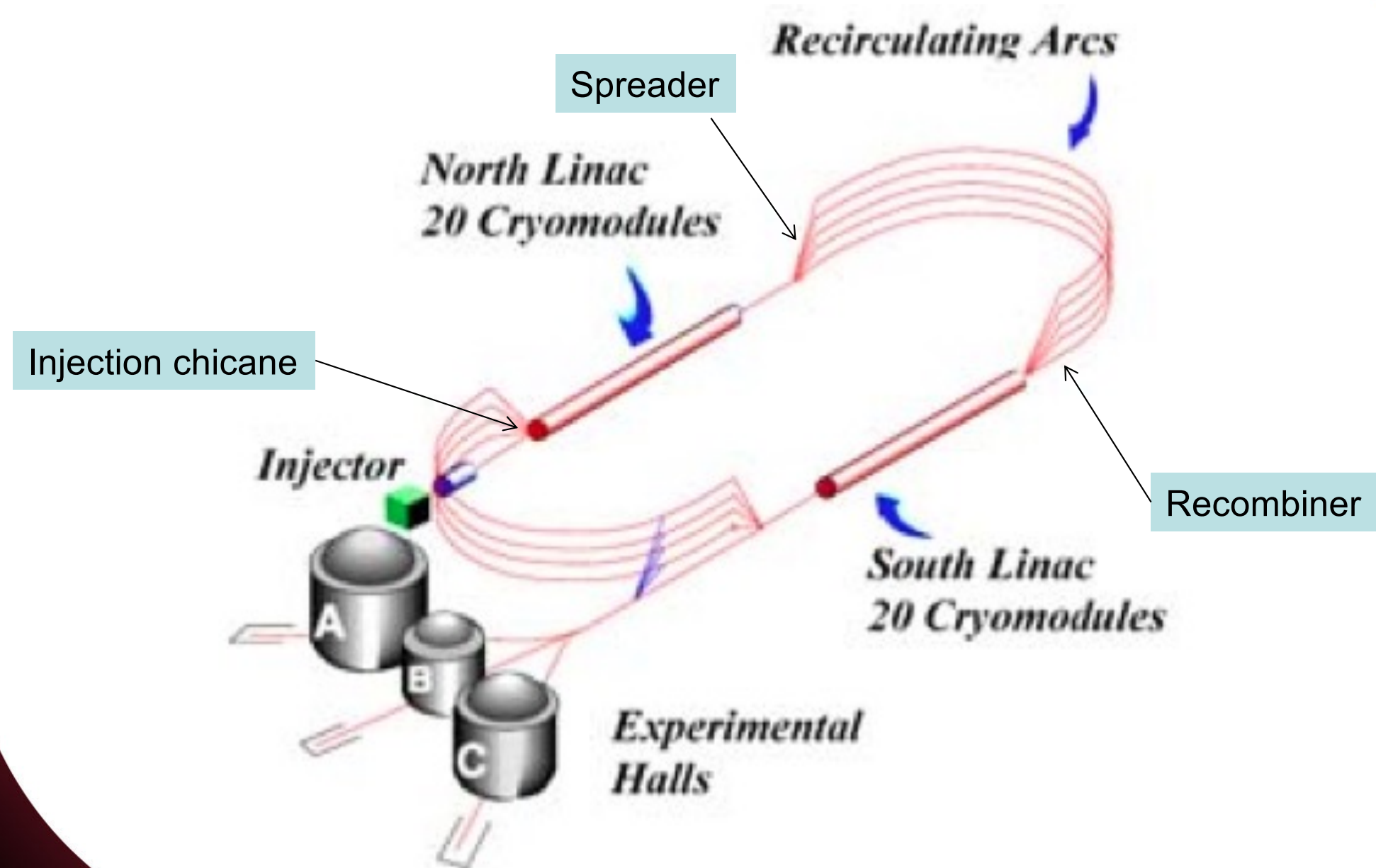
- Divert beam around an obstruction
  - e.g. vertical bypass chicane in Fermilab Main Ring
  - e.g. horizontal injection chicane in CEBAF recirculating linac
  - Essentially a design orbit “4-bump” (4 dipoles)
- Usually need some focusing, optics between dipoles
- Usually design optics to be achromatic
  - Operationally null orbit motion at end of chicane vs changes in input beam energy
- Naively expect  $M_{56} < 0$  (bunch lengthening or decompression)
  - Higher energy particles ( $+\delta$ ) have shorter path lengths
  - But can compress bunches with introduction of longitudinal correlation

# AGS to RHIC (ATR) Transfer Line



The ATR vertical dogleg is not strictly a dogleg since the planes of the AGS and RHIC accelerators are not parallel

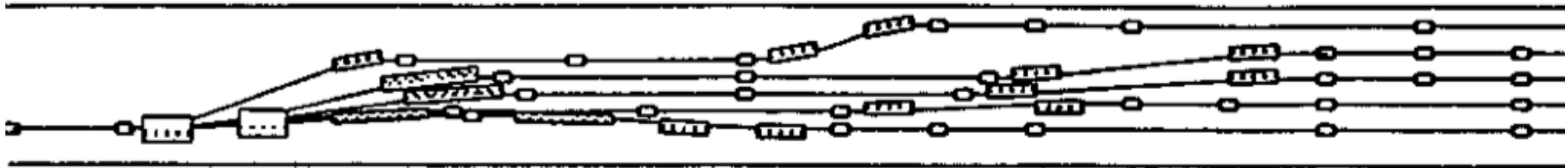
# CEBAF





# CEBAF Spreaders/Recombiners

- Problem: Separate different energy beams for transport into arcs of CEBAF, and recombine before next linac
  - Achromats: arcs are FODO-like, linacs are dispersion-free
  - “I” insertion: 1 betatron wavelength between dipoles
  - Single dogleg: unacceptably high beta functions
  - Two consecutive “staircase” doglegs with same total phase advance was solution

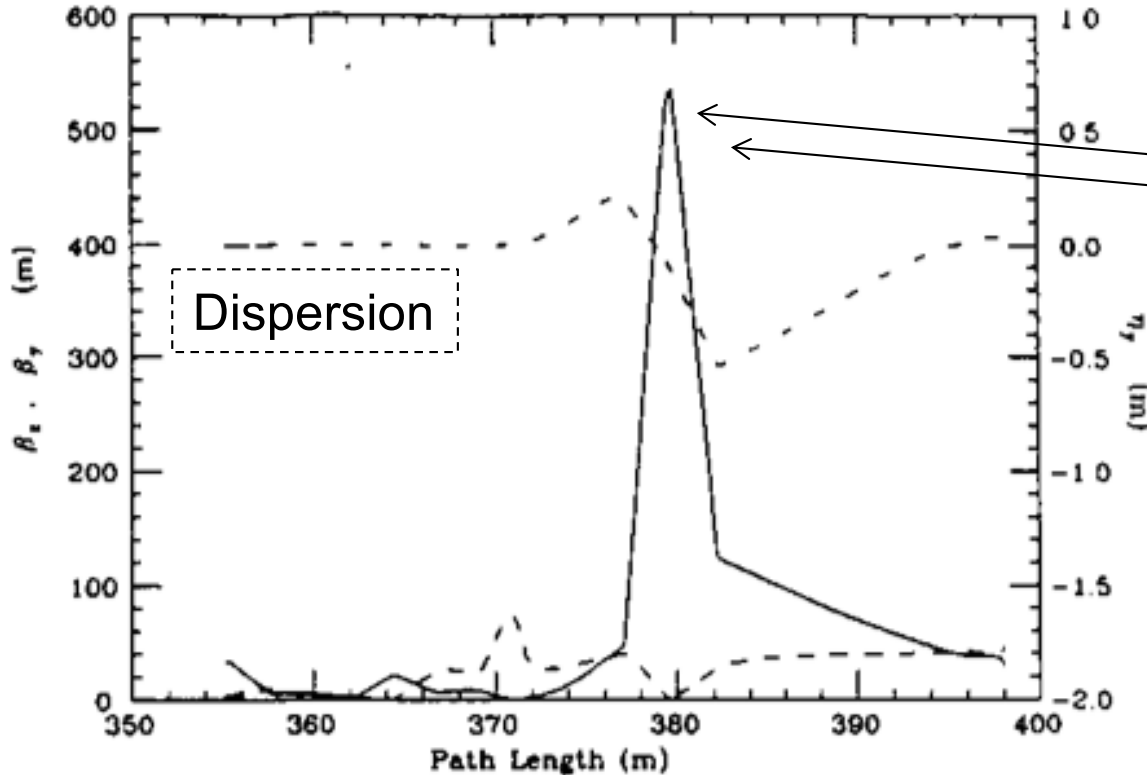


**EAST ARC ELEVATION**

- Still quite a challenge in physical layout of real magnets!

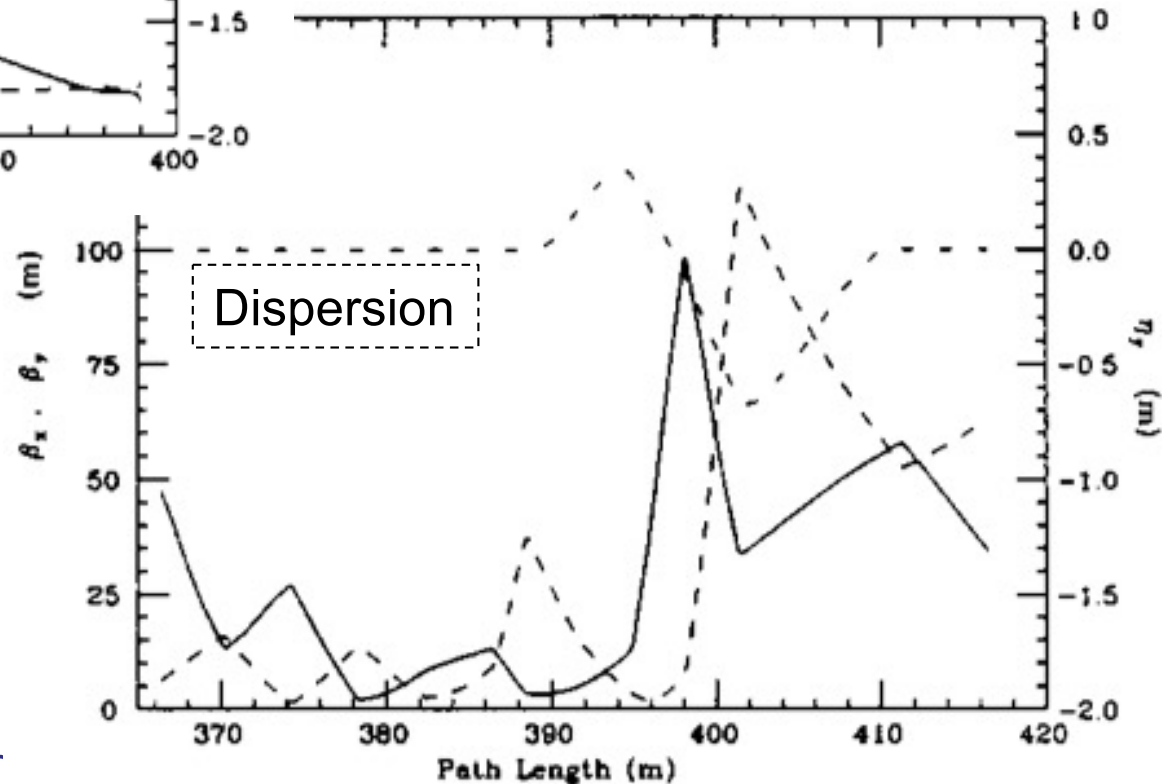
D. Douglas, R.C. York, J. Kewisch, “Optical Design of the CEBAF Beam Transport System”, 1989

# CEBAF Spreaders/Recombiners



"One step" recombiner  
Unacceptably large vertical  
beta function/beam size  
(550 m)

"Staircase" two-step recombiner  
Acceptable beta functions and  
beam sizes in both planes  
(100 m)





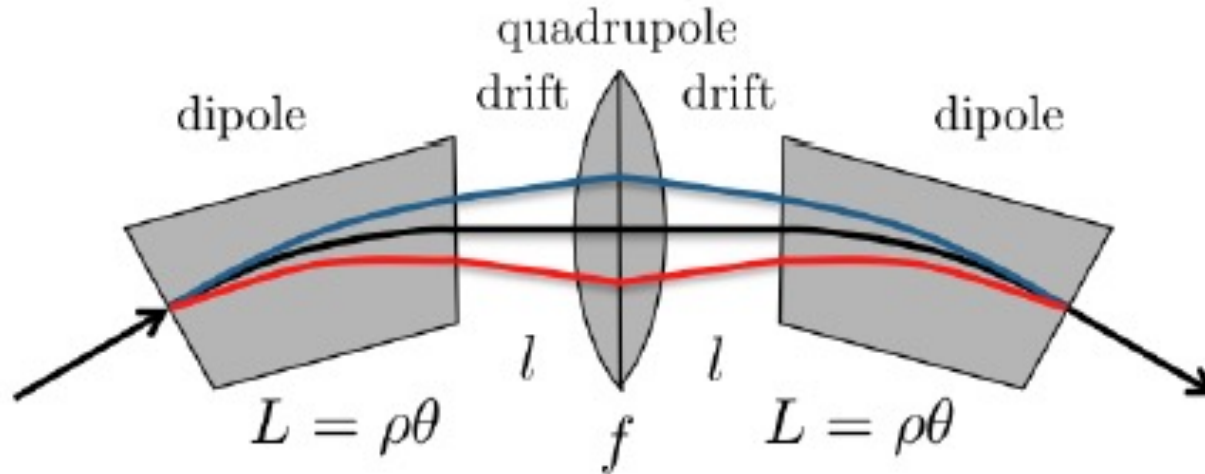
# (xkcd yet again: double bend achromat)

<http://www.xkcd.org/964/>



This is known in accelerator lattice design language as a “double bend achromat”

# Double Bend Achromat (approximate)



- Let's calculate constraints for the double bend achromat

$$M_{\text{dipole}} = \begin{pmatrix} \cos \theta & \rho \sin \theta & \rho[1 - \cos \theta] \\ -\frac{1}{\rho} \sin \theta & \cos \theta & \sin \theta \\ 0 & 0 & 1 \end{pmatrix}$$

Keep lowest-order terms in  $\theta$ , including  $\theta^2$  in upper right term since  $\rho\theta=L$

$$M_{\text{dipole}} = \begin{pmatrix} 1 & L & L\theta/2 \\ 0 & 1 & \theta \\ 0 & 0 & 1 \end{pmatrix}$$

# Double Bend Achromat (approximate)

$$\mathbf{M}_{\text{DBA}} = \begin{pmatrix} 1 & L & L\theta/2 \\ 0 & 1 & \theta \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & l & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & 0 & 0 \\ -\frac{1}{f} & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & l & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{pmatrix} 1 & L & L\theta/2 \\ 0 & 1 & \theta \\ 0 & 0 & 1 \end{pmatrix}$$

$$\mathbf{M}_{\text{DBA}} = \begin{pmatrix} C & S & D \\ C' & S' & D' \\ 0 & 0 & 1 \end{pmatrix}$$

$$C = 1 - \frac{(L+l)}{f}$$

$$S = \frac{(L+l)(2f-L-l)}{f}$$

$$D = \theta \frac{(L+l)(4f-L-2l)}{2f}$$

$$C' = -\frac{1}{f}$$

$$S' = 1 - \frac{(L+l)}{f} = C$$

$$D' = \theta \frac{(4f-L-2l)}{2f} = \frac{D}{L+l}$$

# Double Bend Achromat (approximate)

- The periodic solutions for dispersion for the general M matrix were shown in class earlier today

$$\eta(\text{periodic}) = \frac{[1 - S']D + SD'}{2(1 - \cos \mu)} = 0$$

$$\eta'(\text{periodic}) = \frac{[1 - C]D' + C'D}{2(1 - \cos \mu)} = 0$$

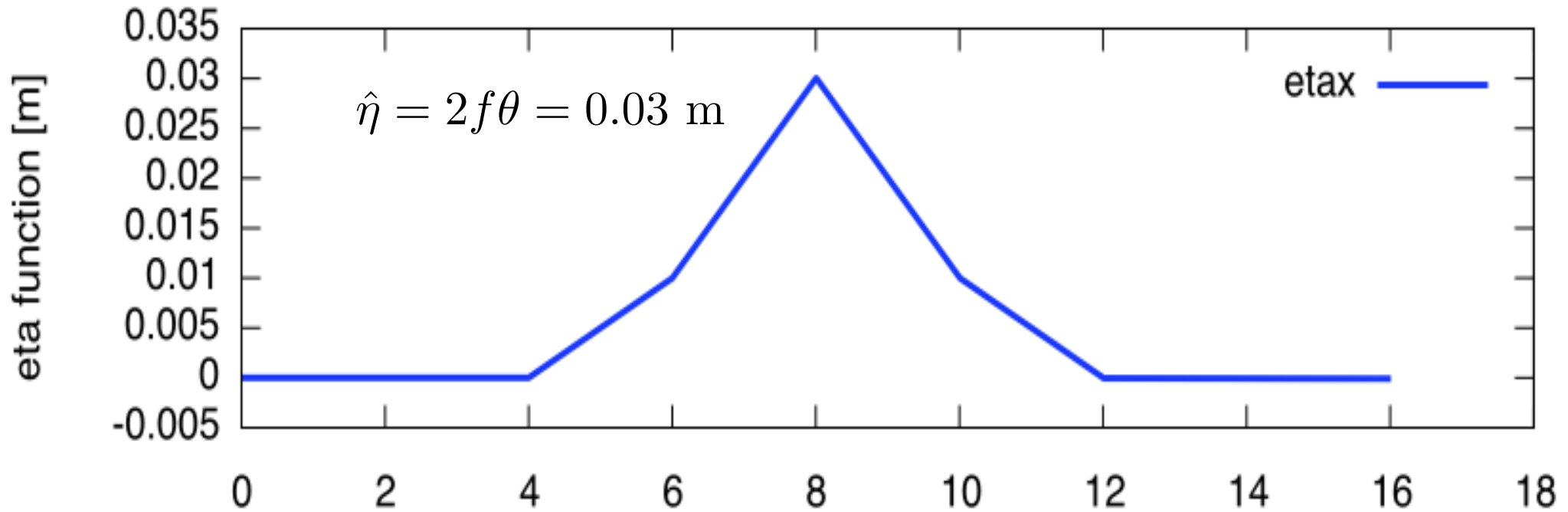
- It turns out that the  $\eta'$  equation is satisfied automatically!
  - This is a consequence of the mirror symmetry of the system
- The  $\eta$  equation is satisfied if  $D=0$ :

$$D = \theta \frac{(L + l)(4f - L - 2l)}{2f} = 0$$

$$\Rightarrow 4f - L - 2l = 0 \quad \Rightarrow \quad f = \frac{L + 2l}{4} \quad \hat{\eta} = \frac{(L + 2l)\theta}{2} = 2f\theta$$

Include link to madx file

## Double Bend Achromat

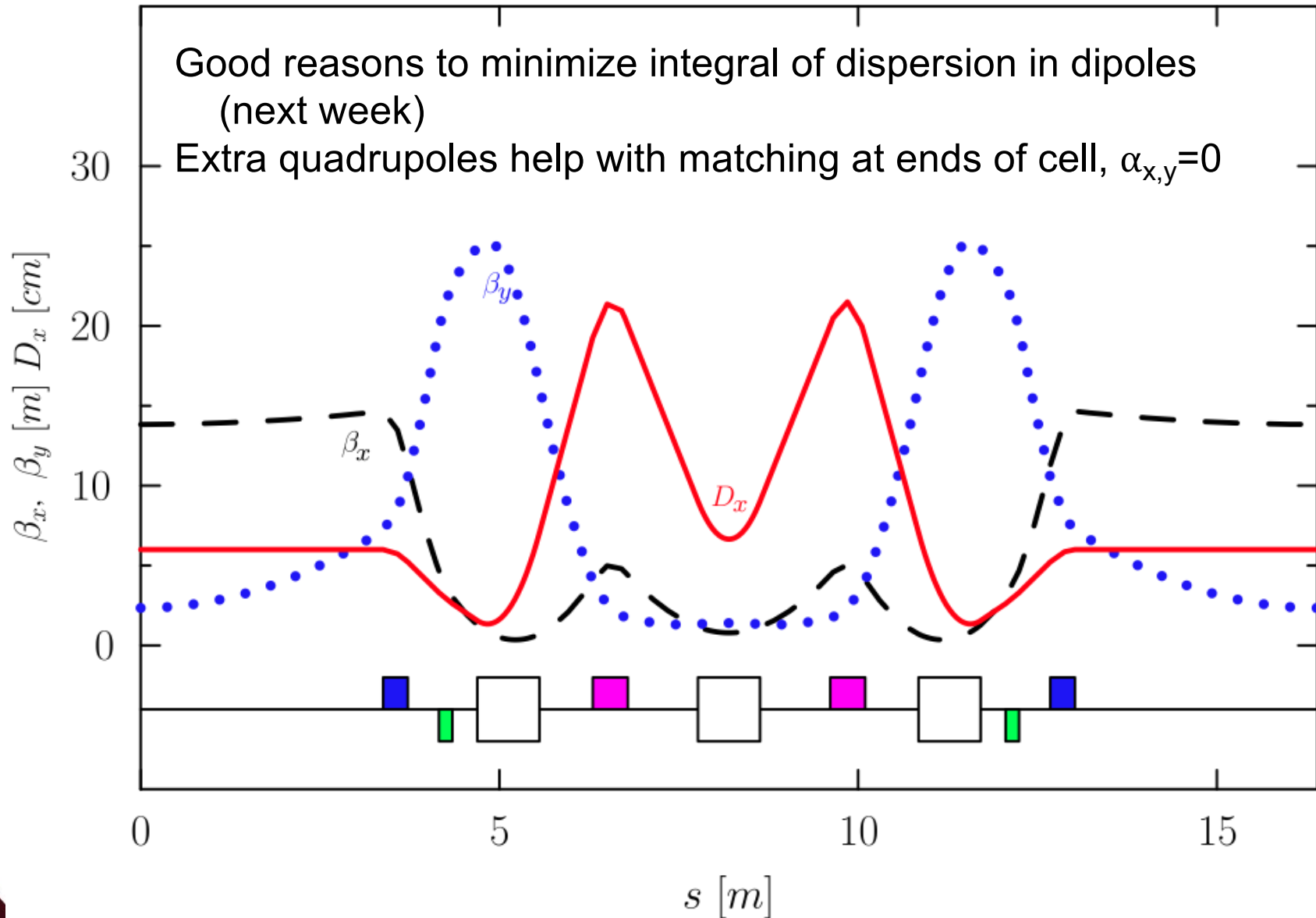


$$L = l = 2 \text{ m} \quad \theta = 0.01 \text{ rad} \quad f = \frac{L + 2l}{4} = 1.5 \text{ m} \quad (KL_{\text{quad}}) = 0.667 \text{ m}^{-1}$$

$$\text{Exact DBA : } f = \frac{l}{2} + \frac{\rho}{2} \tan(\theta/2) \quad \hat{\eta} = \rho(1 - \cos \theta) + l \sin \theta$$

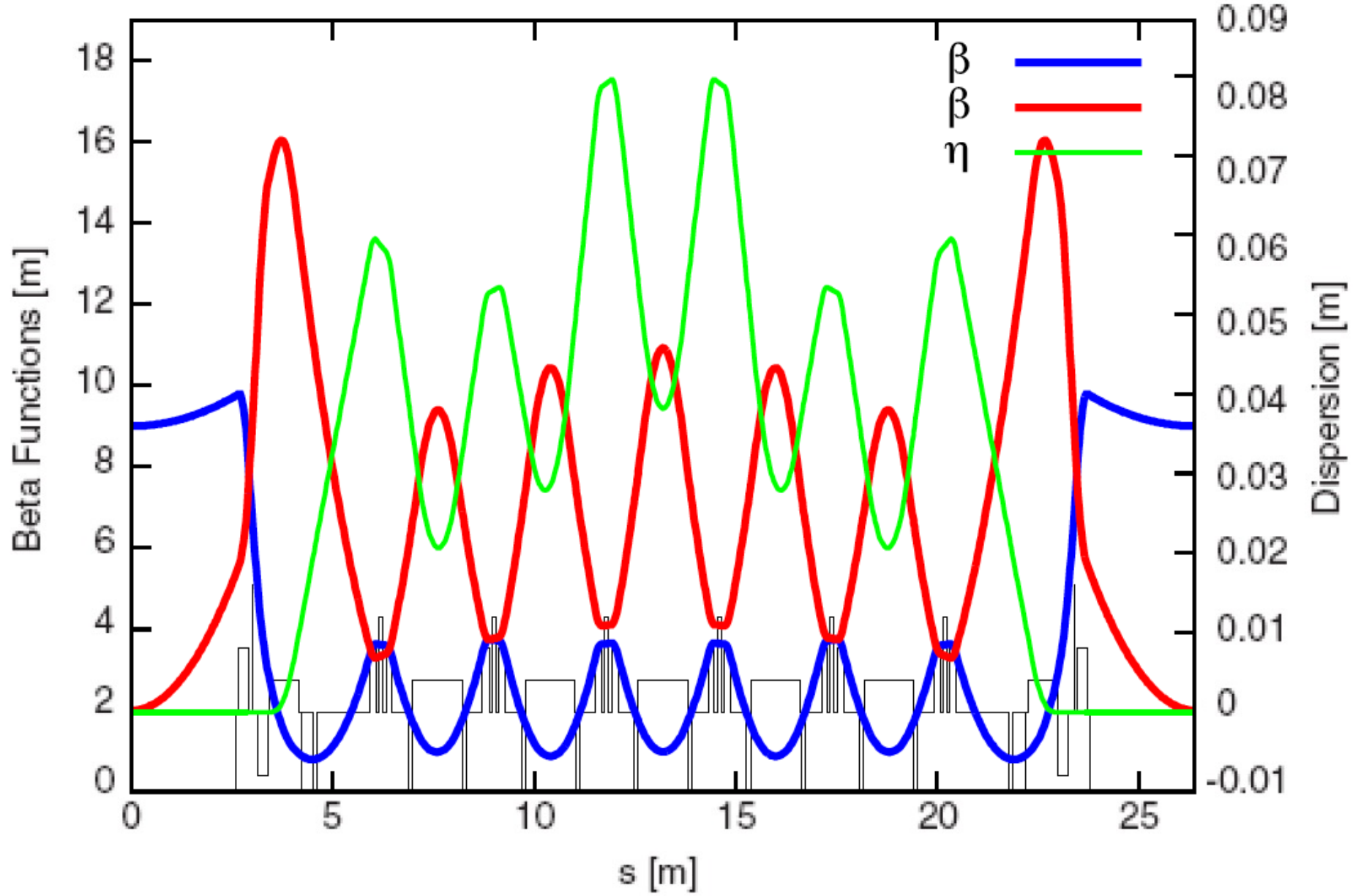
- DBA is also known as a Chasman-Green lattice
  - Used in early third-generation light sources (e.g. NSLS at BNL)
  - More after we discuss synchrotron radiation,  $\mathcal{H}$  functions

# Triple Bend Achromat Cell (ALS at LBL)



L. Yang et al, Global Optimization of an Accelerator Lattice Using Multiobjective Genetic Algorithms, 2009

# MAX-IV 7-Bend Achromat





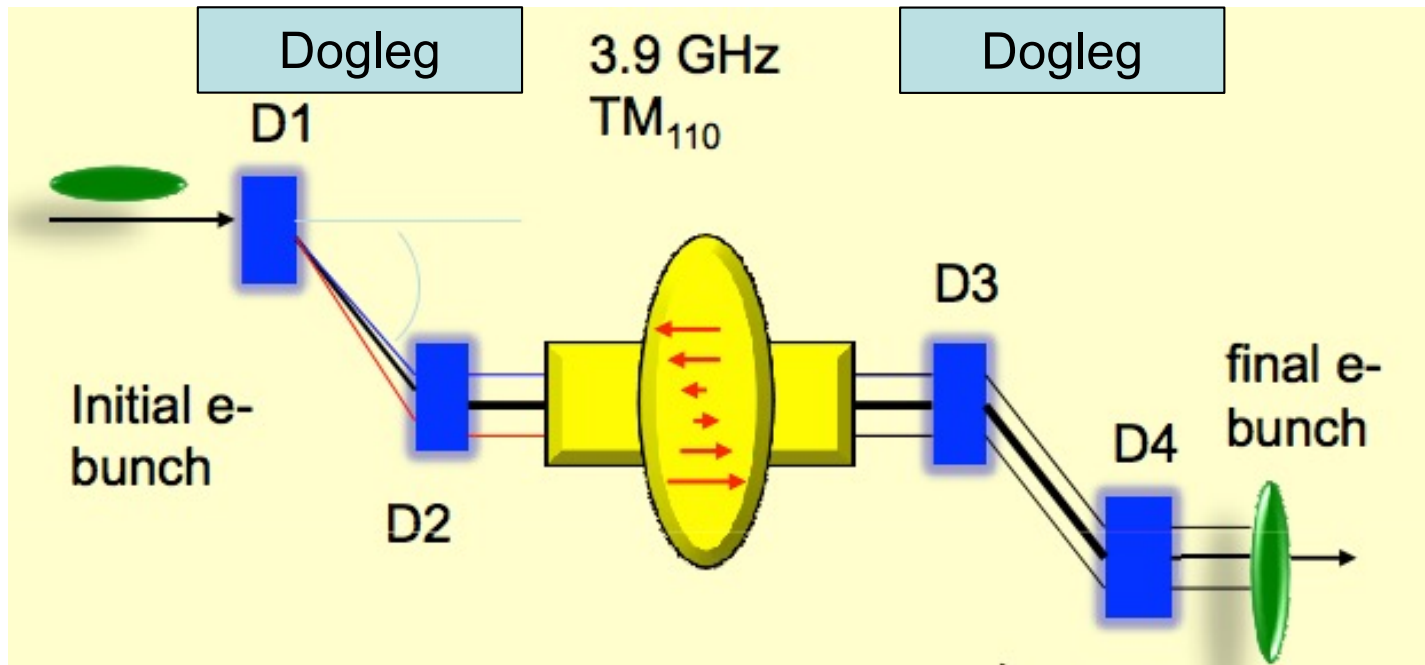
# Transverse/Longitudinal Emittance Exchange

- X-ray FELs demand ultra-low transverse emittance beam\*
- State-of-the art photo-injectors can generate low 6-D emittance. Typically asymmetric emittances. Emittance exchange can swap transverse with the longitudinal emittance.
- Allows one to convert transverse modulations to longitudinal modulations : Beam shaping application
- Can also be used to suppress microbunching instability\*\*

J.C.T. Thangaraj, Experimental Studies on an Emittance Exchange Beamline at the A0 Photoinjector, 2012



# Fermilab A0 Emittance Exchanger



$\theta$  : Bending angle  
 $\eta$  : dogleg dispersion  
 $L$  : dogleg length  
 $L_c$  : RF cell length

$$\mathbf{M} = \begin{pmatrix} 1 & \frac{L_c}{4} & -\frac{(4L+L_c)}{4\eta} & \eta - \frac{\theta(4L+L_c)}{4} \\ 0 & 1 & -\frac{1}{\eta} & -\theta \\ -\theta & \eta - \frac{\theta(4L+L_c)}{4} & 1 + \frac{\theta L_c}{4\eta} & \frac{\theta^2 L_c}{4} \\ -\frac{1}{\eta} & -\frac{4L+L_c}{4\eta} & \frac{\theta L_c}{4\eta^2} & 1 + \frac{\theta L_c}{4\eta} \end{pmatrix} \begin{pmatrix} x \\ x' \\ z \\ \delta \end{pmatrix}$$

J.C.T. Thangaraj, Experimental Studies on an Emittance Exchange Beamline at the A0 Photoinjector, 2012

# TM110 RF Cavity Mode

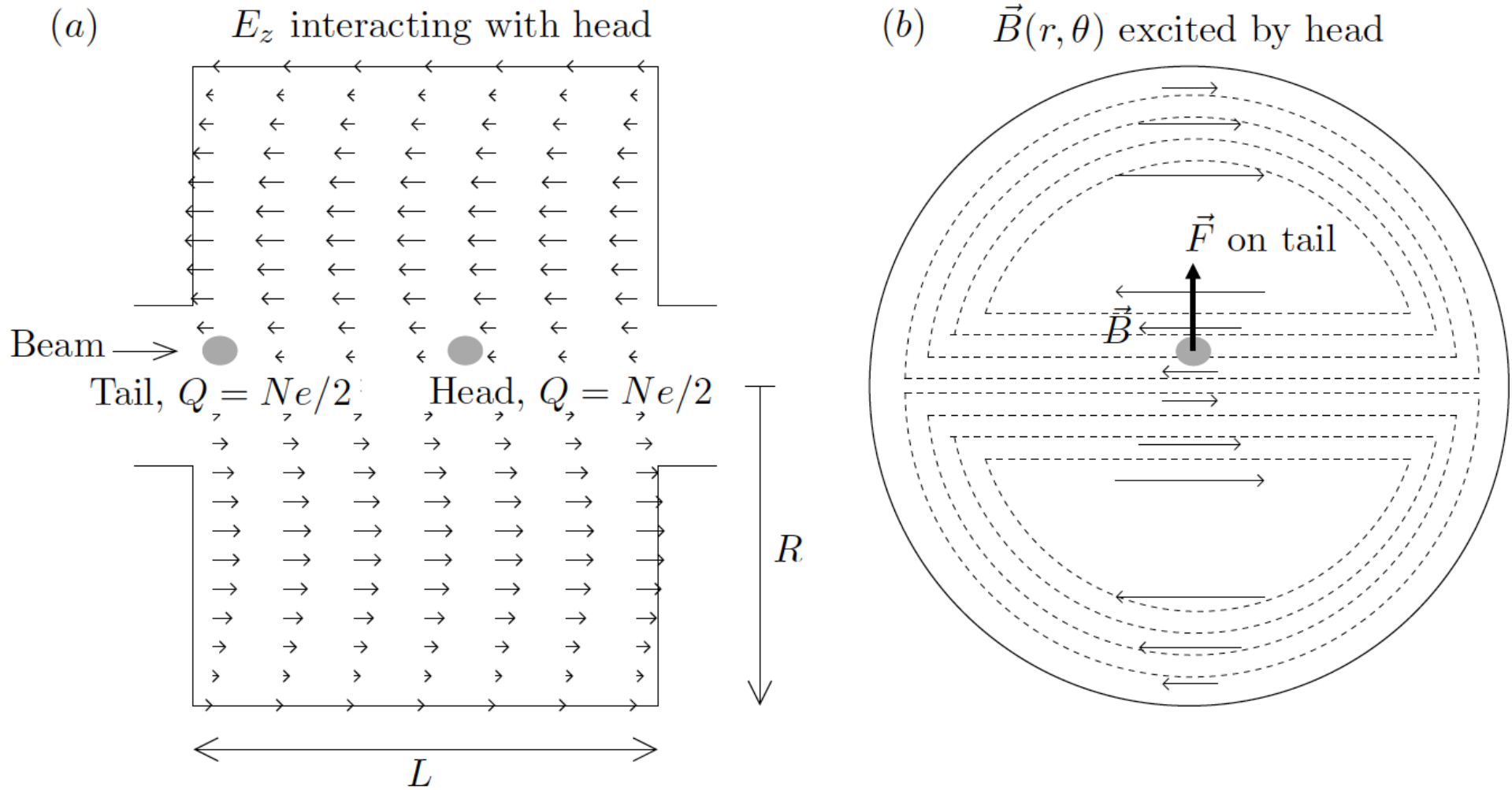


Figure 14.6 in textbook

# Chicane Style Emittance Exchange (2011)

DAO XIANG *et al.*

Phys. Rev. ST Accel. Beams **14**, 114001 (2011)

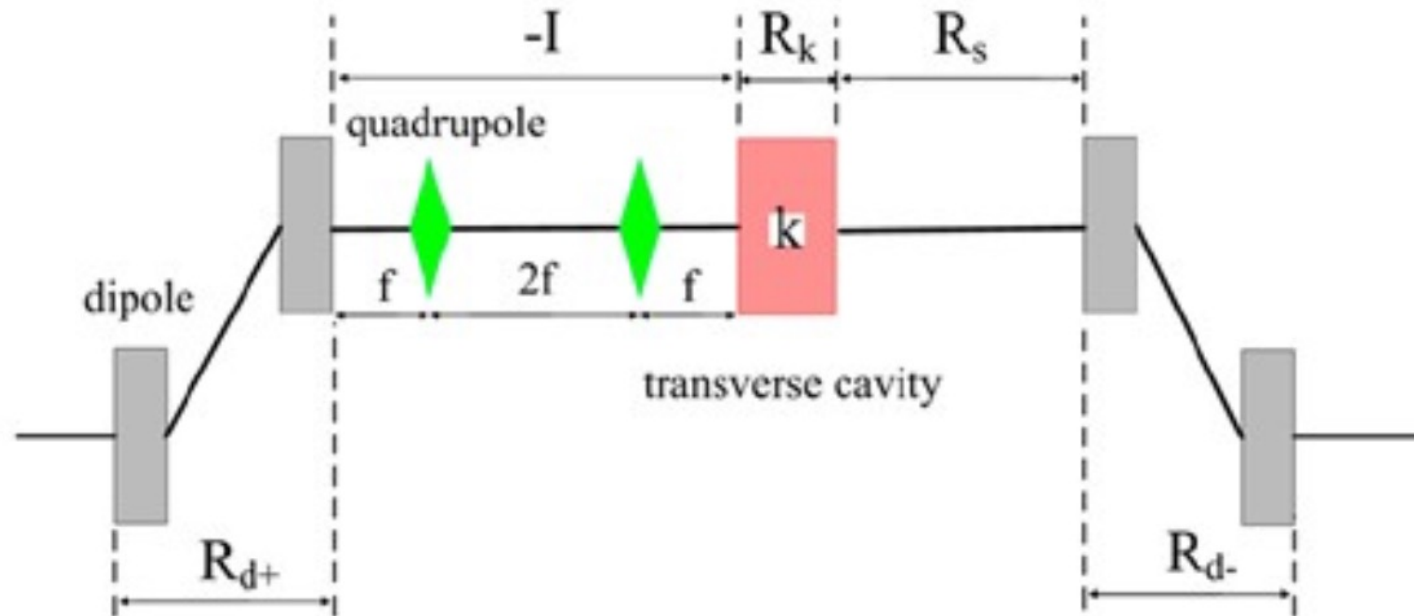
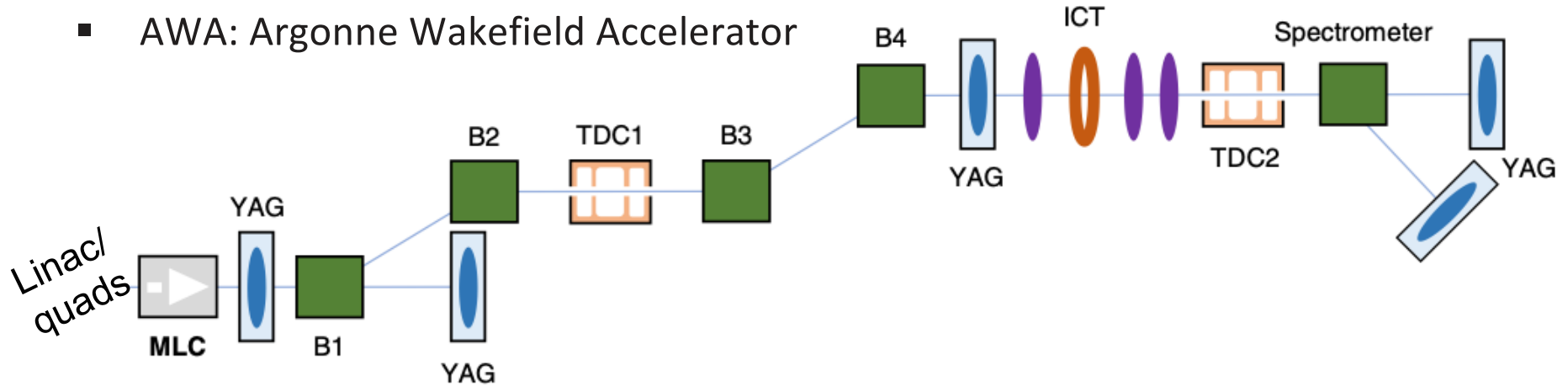


FIG. 2. A chicane-type exact EEX beam line. Two quadrupoles (green diamonds) are put upstream of the transverse cavity to reverse the dispersion.

- Reversing dispersion before the TM cavity allows you to flip the second dogleg to make a chicane
  - More transversely compact emittance exchange

# AWA Longitudinal Shaping with EEX (2023)

- Majernik et al., [PHYS. REV. ACCEL. BEAMS 26, 022801 \(2023\)](#)
- AWA: Argonne Wakefield Accelerator



- Shape beam transversely using multi-leaf collimator
  - Near-arbitrary transverse beam shapes: EEX converts to longitudinal
  - Longitudinal pulse shaping is important for e.g. FELs, wakefield accelerators

